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Characteristics of a 3-Hinged Arch

- Statically determinate can be calculated with statics
- Movement or settling of foundations will not alter member stresses
- Small fabrication errors in length do not affect internal stresses
- Hinge placement can reduce internal stresses



Gallery of the Machines, 1889 Paris Architect: Ferdinand Dutert Engineer: Victor Contamin

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3-Hinged Arch analysis

procedure

- 1. Determine all external loads.
 - find resultants of distributed loads (e.g. wind, snow, dead load)
- 2. Calculate vertical end reactions.
 - sum moments at each reaction
- 3. Draw an FBD of each side of the arch.
 - split at the hinge
- 4. Find the horizontal reactions.
 - sum moments at hinge
- 5. Find internal moments.
 - cut additional FBDs (e.g., at the knees)



3-HINGED ARCH



3-Hinged Arch even supports example 1

- 1. Determine all external loads find resultants of distributed loads (e.g. wind, snow, dead load)
 - Wind causes a pressure load, normal to the surface of the structure.
 - Wind can be positive pressure or negative suction and the pressure varies depending on the slope of the surface.
 - The pressure is typically expressed in PSF which translates to a PLF load on the members.

In this example with bents @ 10 ft. o.c.:

- wind on the wall is 25 PSF = 250 PLF
- wind on the roof is 10 PSF = 100 PLF

An FBD is drawn for a single bent (arch) of the structure.

The resultants of the uniform PLF loads are found in lbs.



3-Hinged Arch even supports example 1

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- 2. Calculate the vertical end reactions.
 - sum moments at each reaction.

An FBD is drawn for a single bent of the structure.

The resultants of the uniform PLF loads are found and broken into horizontal and vertical components.

If the reactions are on the same horizontal, summing moments at either reaction will find the vertical component of the opposite reaction.



 $\Sigma M @ A to get By = 1.36 k \downarrow$ $\Sigma M @ B to get Ay = 3.44 k \downarrow$

$$\begin{split} \Sigma MeA &= 0 = 5^{\kappa} (10^{\prime}) - 0.8^{\kappa} (24^{\prime}) - 2.4^{\kappa} (12^{\prime}) - 24^{\kappa} (36^{\prime}) + 0.8^{\kappa} (24^{\prime}) + B_{y} (48^{\prime}) \\ B_{y} &= 1.36^{\kappa} \\ \Sigma MeB &= 0 = 5^{\kappa} (10^{\prime}) + 2.4^{\kappa} (36^{\prime}) + 2.4^{\kappa} (12^{\prime}) - 0.8^{\kappa} (24^{\prime}) + 0.8^{\kappa} (24^{\prime}) - A_{y} (48^{\prime}) \\ A_{y} &= 3.44^{\kappa} \end{split}$$

3-Hinged Arch even supports example 1

- 3. Draw an FBD of each side of the arch.
 - split at the hinge.
- 4. Find the horizontal reactions
 - sum moments at hinge.

$$\Sigma M_{c} = 0 = 2.4^{\kappa} (12') + 0.8^{\kappa} (4') - 5^{\kappa} (18') - 3.44^{\kappa} (24') + A_{x} (28')$$
$$A_{x} = 5.02^{\kappa} \longleftarrow$$

 $\sum_{k=0}^{\infty} M_{c} = 0 = -2.4^{k} (12') - 0.8^{k} (4') + 1.36^{k} (24') - B_{x} (28')$ $B_{x} = 0.02 K \longrightarrow$



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28'

3-Hinged Arch even supports example 1

- 5. Find internal moments
 - cut additional FBDs (e.g., at the knees).



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24

Ay= 3.44 K

24'

left wall

right wall

$$\sum M_{L} = 0 = +5.02^{\kappa} (20') - 5^{\kappa} (10') - M_{L}$$

$$M_{L} = 50.4'^{-\kappa}$$

$$\sum M_{R} = 0 = -0.02^{\kappa} (20') + M_{R}$$

$$M_{R} = 0.4'^{-\kappa}$$

3-Hinged Arch even supports example 1

Internal moments can be calculated taking appropriate sections and FBD's.

The moment diagram is traditionally drawn on the tension side (the opposite of the convention used for beams).

Tension on the inside is called a positive moment regardless of rotation direction.





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Ah



$$-A_{H}(0.5') + 2880 = A_{H}(1.5') + 1440$$

 $A_{H} = 720^{*}$

2. Solve the two equations for Ah and Av

$$A_v = A_u (1.5) + 1440$$

 $A_v = 720(1.5) + 1440$
 $A_v = 2520^*$

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3-Hinged Arch Uneven Supports example 2

240 PLF W=240 PLF × 12' W=2800* 4. Repeat for right side or sum vertical and horizontal forces. 6' 12' 12' 12' $\Sigma F_v = 0 = 2520^* - 2880^* - 2880^* + B_v$ $B_v = 3240^*$ 24' ΣFH=0= 720*-BH By = 720* University of Michigan, TCAUP Structures I Slide 15 of 19 3-Hinged Arch Uneven Supports example 2 5. Cut FBDs at knees to find internal moments 72C • BH 720* 2520 left knee right knee EMCLEFT KHEE = 0 ML - 720*(12')=0 M1 = 8640 1- * 12' EMERIGHT KNEE = O -MR+720*(24')=0 MR = 172801-* 24' 3240.0 Ib

Sign Convention for Frames

Draw the moment on the tension side of the member.

The traditional convention is:



Examples and Details





Center Hinge

Sydney Harbour Bridge





Hinged Glulam Timbers

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Keystone Wye Bridge

Glulam arches, spanning 160 ft. built 1967-68 in South Dakota



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